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THE TENSILE PROFERTIES OF SOME STRUCTURAL MATERIALS.

IN THE TENSERATURE RANGE 295°K TO 20°K

PART II ALIMINUM ALLOY SHEET 1748 WP

by

P. Midgley

R. W. Thackray

July 1963

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Technical Memorandum 471

July 1968

THE TENSILE PROPERTIES OF SOME STRUCTURAL MATERIALS IN THE TEMPERATURE RANGE 293°K TO 20°K; PART II, ALIMINIUM ALLOY SHEET D74S WP

bу

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R. W. Thackray

SUMMARY

The tensile properties of the aluminium alloy sheet D74S WP have been measured at temperatures of 293, 77 and 20°K. Plain and notched specimens from the longitudinal and transverse directions of the sheet were tested.

The results indicate that the alloy can be used in structures operating at temperatures down to 77°K.

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1 INTRODUCTION

The use of liquid hydrogen, fluorine and oxygen, with boiling points of 20°K, 86°K and 90°K respectively, as propellents in high energy propulsion systems, and also the application of other liquid gases in commercial projects has led to an increased interest in the physical and mechanical properties of constructional materials over a range of temperatures from 293°K down to 20°K.

The mechanical properties of materials at these extremely low temperatures vary considerably. The strength of most materials increases as the temperature decreases, but unfortunately this is usually accompanied by a decrease in toughness, i.e. a reduction in the material's resistance to brittle failure.

The main requirements that any material must fulfil before it can be applied in highly stressed components or structures operating at cryogenic temperatures are that it should

- (a) have a high strength/density ratio,
- (b) have adequate toughness
- (c) be weldawle and easily fabricated, and
- (d) be readily available, preferably at low cost.

Much effort has been expended in the U.S.A. on evaluating both metallic and non-metallic materials over the temperature range 293°K down to 20°K^{1,2,3,4}. It is unfortunate that, in general, there is no direct correlation between the chemical and mechanical specifications of U.S. and U.K. materials. Small changes in chemical composition and processing can give rise to marked differences in the mechanical properties of a material at low temperatures. For this reason it is necessary to measure the properties of U.K. materials which have potential applications. This Memorandum, one of a series⁵, presents the results obtained from the evaluation of D74S WP aluminium alloy sheet.

2 EXPERIMENTAL

2.1 Facilities

The low temperature testing laboratory and experimental equipment for measuring the tensile properties of materials over the temperature range 293°K down to 20°K have been described fully elsewhere 6.

2.2 Material

174S, an alloy of aluminium-4.5% zinc - 1.25% magnesium, was supplied by Alcan Industries Ltd. In the fully heat treated condition it has an ultimate tensile strength varying from 300 MM/m² (19 ton f/in²) to 380 MM/m² (25 ton f/in²) at 293°K. The chemical composition of the alloy evaluated is given in Table 1 along with the equivalent French alloy AZ5G for comparison⁷.

Provided that the correct welding procedures are employed, 1748 can be readily welded. Comparatively high joint efficiencies can be obtained in the weld region due to a recovery in strength of the heat-affected zone by natural ageing. If a full heat treatment is carried out after welding 100 per cent joint efficiencies are possible.

2.3 Test specimens

Two types of test specimen, shown in Fig.1, were used. A "pipped" test piece was used to determine the tensile properties, and a "notched" test piece for the evaluation of toughness.

2.3.1 "Pipped" test piece

The pips on the gauge length were used to locate and attach the extensometer arm assembly simply and accurately. Specimens were taken from the sheet in both the longitudinal and transverse directions relative to the direction of rolling during manufacture. For each configuration, two specimens were tested at 293°K and three specimens at 77°K (the boiling point of liquid nitrogen) and at 20°K. In all tests the strain rate was 0.005 minute⁻¹ to determine the proof stress and subsequently 0.05 minute⁻¹ to fracture.

2.3.2 "Notched" test piece

The root radius of the notches was 0.05-0.075 mm (0.002-0.003 inch), giving a stress concentration factor (K_t) of 6.3. This value of K_t was selected because

- (i) it had been used extensively in U.S. programmes evaluating material behaviour at cryogenic temperatures, and
- (ii) it is thought to be more sensitive in differentiating between tough and brittle materials³.

3 RESULTS

The results of tensile tests for unnotched specimens tested in the longitudinal and transverse directions are given in Table 2, and for notched specimens in Table 3. Comparative data on an equivalent French material, AZ5G 7,

are presented in Table 4. The variation in the tensile properties of D74S WP with temperature are shown in Fig.2, and the appearance of the fractured test pieces in Figs.3 and 4.

4 DISCUSSION

The properties of D74S WP in the longitudinal and transverse directions showed a similar variation with temperature. The ultimate tensile strength increased markedly from 305.8 MN/m² (19.8 ton f/in²) at 293°K to 514.3 MN/m² (33.3 ton f/in²) at 20°K, whilst the variation in proof stress was smaller, increasing from 264.1 MN/m^2 (17.1 ton f/in²) to 332.1 MN/m^2 (21.5 ton f/in²) over the same temperature range. The ratio of Notched Tensile Strength/ Ultimate Tensile Strength (N.T.S./U.T.S.) was greater than unity down to approximately 50°K, but at 20°K it had decreased to a value of 0.79 and 0.84 for longitudinal and transverse specimens respectively. A value of the N.T.S./U.T.S. ratio of less than unity is considered to be an indication that the material is becoming brittle and less resistant to crack propagation. This latter tendency is confirmed by the appearance of the fracture surfaces of the notched test pieces (Fig.4). Specimens tested at 293°K failed in a completely ductile manner by shear accompanied by plastic deformation. The fracture surfaces of specimens broken at 77°K and 20°K, however, comprised two regions; the first, adjacent to the root of the notch, indicates that the crack had initially propagated in a brittle manner under plane strain conditions, and the second region that the mode of propagation had changed to a ductile shear mechanism associated with plane stress conditions. degree of brittle fracture in the test piece increases with decreasing temperature indicating that the material becomes more brittle as the temperature is lowered.

An unusual feature of the results is the increase in total elongation of the specimen with decreasing temperature, ranging from 10 per cent at 293°K to a maximum of 27 per cent at 20°K. From the discussion of the results and the conclusion already reached that the material becomes more brittle at low temperatures, a decrease in total elongation would be expected. The reason for this discrepancy is not obvious. It could be caused by the notched specimens being broken in a bi-axial stress system, whereas in the conventional tensile test the specimen is subjected to a uni-axial stress. Attention should be given therefore to the influence of multi-axial stresses on the brittle behaviour of aluminium alloys and components at cryogenic temperatures.

5 CONCLUSIONS

The medium strength aluminium alloy sheet 1745 WP can be used safely in the construction of components operating at temperatures down to 77°K. A more extensive testing programme would be required before it could be decided whether the material was suitable for use at temperatures below 77°K.

The trend in the properties of D74S WP with decreasing temperature from 293°K to 20°K, for both longitudinal and transverse specimens can be summarised by the following characteristics:

- (a) a slight increase in the 0.2 per cent proof stress from 260 MN/m^2 to 330 MN/m^2 .
 - (b) A more marked increase in the U.T.S. from 305 MN/m^2 to 515 MN/m^2 .
- (c) A pronounced increase in total elongation from 10 per cent to 27 per cent.
 - (d) A N.T.S./U.T.S. ratio greater than unity above 50°K.

Table 1

CHEMICAL COMPOSITION OF D74S AND

AZ5G ALUMINIUM ALLOYS

Material		. Q	uantity	of allo	oying el	Lement,	per cer	nt	
Marcerian	Fe	· Cu	Si	Min	Mg	Ti	Cr	Zn	Zr
D74S	0.28	0.01	0.11	0.25	1.37		0.13	4.53	
AZ5G	0.25	0.01	0.07	0.23	1,15	0.03	0.19	4.79	0.16

Table 2
TENSILE STRENGTH OF D74S WP ALUMINIUM ALLOY
THICKNESS 1.2 mm (0.048 in)

Temp.,	Proof	stress, 1	M/m ²	U.T.S.,	Elongation on 50.8 mm,	Modulus of elasticity,	
°K	0.1%	0.2%	0.5%	MN/m ²	per cent	GN/m ²	
		Longitud	inal (in	direction of	rolling)		
293 77 20	259 287 323	264 295 334	269 301 343	306 389 514	11.0 21.6 33.4	68.2 76.1 75.8	
Transverse (perpendicular to direction of rolling)							
293 77 20	250 279 320	258 292 332	266 304 346	304 392 528	10.0 19.4 27.1	68.4 69.8 72.0	

Temp.,	Proof st	ress, ton	f/in ²	U.T.S., 2 ton f/in	Elongation on 2 inches, per cent	Modulus of elasticity, 102 ton f/in2	
	0.12			direction of		100 100 17 100	
20 196 253	16.8 18.6 20.9	17.1 19.1 21.5	17.4 19.5 22.2	19.8 25.2 33.3	11.0 21.6 33.4	4.42 4.93 4.91	
	Transverse (perpendicular to direction of rolling)						
20 -196 -253	16.2 18.1 20.7	16.7 18.9 21.4	17.2 19.7 22.4	19.7 25.4 34.2	10.0 19.4 27.1	4.43 4.52 4.66	

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Table 3

NOTCHED TENSILE STRENGTH OF D74S WP ALUMINIUM ALLOY
THICKNESS 1.2 mm (0.048 in)

Temp.,	Notched tensile strength (N.T.S.), MN/m ²	N.T.S. U.T.S.	N.T.S. 0.2% proof stress
	Longitudinal (in di	rection of	'rolling)
293 77 20	337 428 406	1.10 1.09 0.79	1.27 1.45 1.22
Tran	sverse (perpendicular	to direct	ion of rolling)
293 77 20	349 429 442	1,15 1,11 0,83	1.35 1.47 1.34

Temp.,	Notched tensile strength (N.T.S.), ton f/in ²	N.T.S.	N.T.S. 0.2% proof stress			
	Longitudinal (in di	rection of	rolling)			
20 -196 -253	21.8 27.7 26.3	1.10 1.09 0.79	1.27 1.45 1.22			
Transverse (perpendicular to direction of rolling)						
20 -196 -253	22.6 27.8 28.6	1.15 1.11 0.83	1.35 1.47 1.34			

Table 4

MECHANICAL PROPERTIES OF THE ALUMINIUM ALLOYS

D748 WP AND AZ5G-T6

Temp.,	Direction	. 6 7 2 6 4 6 7	0.2% pr	0.2% proof stress		U.T.S.	11.	H.T.8.	Elongstion,
×.	of test	מספגיסד	MV/m ^{2;}	ton f/in ²	MN/m ²	tor f/in ²	MN/mg	ton f/in ²	per cent
	Long.	dm shla	792	1.71	90€	19.8	337	81.8	0.11
293	Trans.	D748 WP AZ5G-T6	258 324	16.7 21.0	304 373	19.7	>45 488*	22.6 27.3*	10.0
	Long.	am shla	295	19.1	684	25.2	428	27.7	9" 18
12	Trans.	D748 WP AZ5G—T6	292 412	18.9 26.7	398 520	25.4 33.7	429 540*	27.8 35.0*	19.4
	Long.	D74S WP	334	21.5	514	33.3	9017	26.3	7.66
ର	Trans.	<i>D7</i> 48 WP A25g-16	332 432	4.52	528 628	34.8 40.7	442 618*	28.6 40.04	207.1 40.1

*denotes Kt = 4.8

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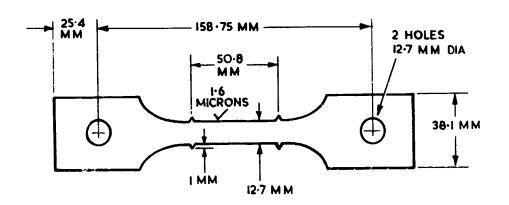
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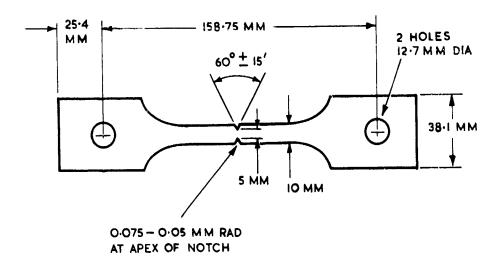
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(A) PIPPED TEST PIECE



(B) NOTCHED TEST PIECE

FIG. 1 TENSILE TEST PIECES

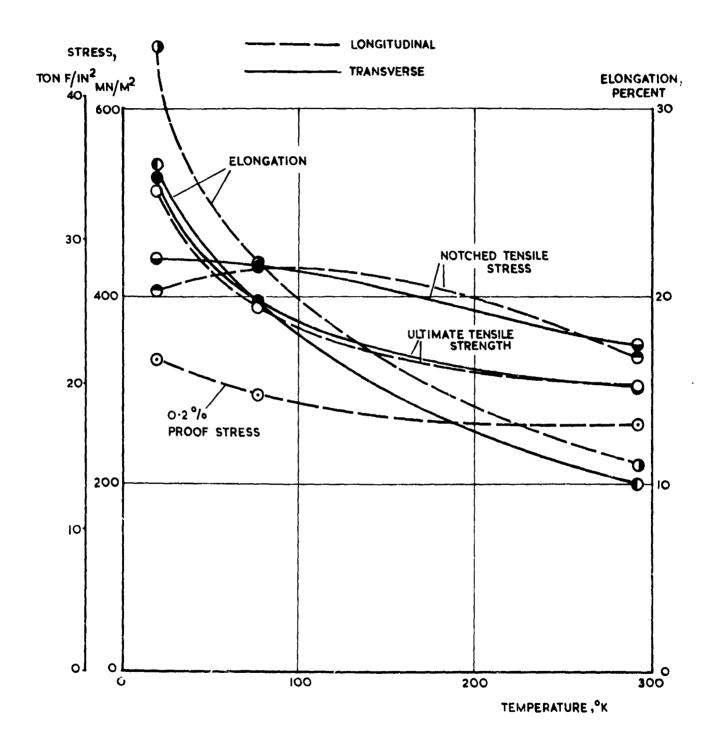
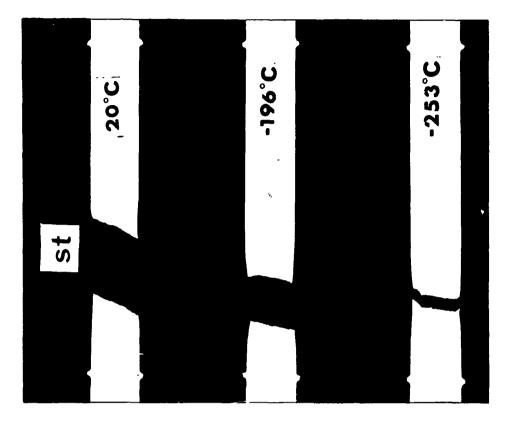
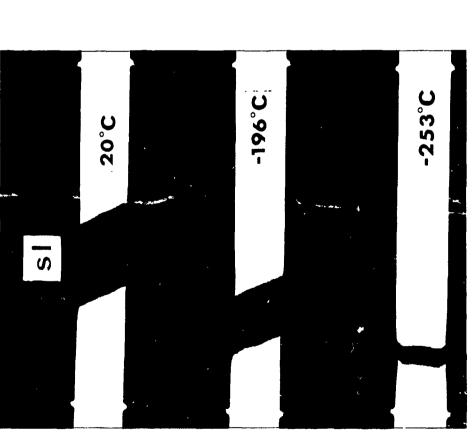


FIG.2 VARIATION IN TENSILE PROPERTIES OF D745 WP WITH TEMPERATURE

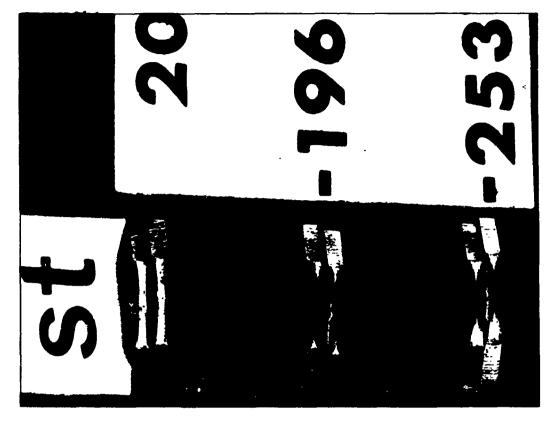


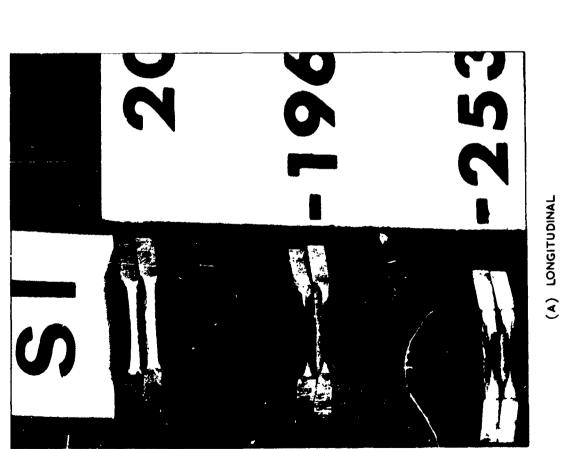


(B) TRANSVERSE

(A) LONGITUDINAL

FIG.3 TENSILE TEST PIECES AFTER TESTING AT DIFFERENT TEMPERATURES





(B) TRANSVERSE

FRACTURE SURFACE OF NOTCHED TEST PIECE FIG.4



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